

# Development of Antenna for Microwave Imaging Systems for Breast Cancer Detection

Samira Al'Habsi\*, Thuraiya Al'Ruzaiqi, Khalid Al'Hadharami and Sreelakshmi T. Gopinathan

Department of Electronics and Communication, Middle East College, Sultanate of Oman

## Abstract

**Motivation:** Breast cancer is a major health problem globally for women causing an appreciable percentage of the yearly female death. Microwave imaging is a promising method in biomedical applications such as breast cancer detection due to its good penetration property, non-ionizing and non-invasive nature which has the potential to be a complementary modality to standard mammography. In this paper, An UWB Microstrip-fed Vivaldi antenna for microwave imaging systems aimed for an early breast cancer detection is developed.

**Results:** The Vivaldi antenna is designed to operate between 8.821 to 22.30 GHz with dimensions of 44.85 × 25.28 mm that permits good radiation within the frequency range. To achieve UWB performance, Taconic TLC-32 substrate which has relative permittivity of 3.2 has been used to simulate the antenna by using Antenna Magus Software. The simulation results show that the return loss is better than -10dB within the range of 7.143 GHz to 24.60 GHz with the maximum return loss of -37.56 dB at 18.39 GHz. However, due to difficulties in antenna fabrication at higher frequencies, a low frequency of about 2.4 GHz is considered. Antenna measurements presents good radiation pattern that suit medical imaging systems to detect breast tumors. The amount of reflection is also found to be minimum for the antenna design frequency (2.4 GHz) which appears to be -26.34 db.

**Keywords:** Ultra-wideband (UWB); Microwave imaging; Return loss; Radiation pattern

## Introduction

Microwave imaging for biomedical applications is nowadays of very significant interest, having the potential of providing information about both physiological states and anatomical structures of human tissues. The imaging with microwaves allows non-destructive evaluation of biological tissues due to the non-ionizing nature of microwaves, since changes in the dielectric properties of tissue can be related to their physiological condition. One of the most promising applications deployed is detection of breast tumors [1-4]. This is particularly eligible due to the easy approach of the breast for imaging, as well as the breast anatomy where the fatty tissue (with low loss) has a low attenuation impact on the signal. The contrast in permittivity for different *in-vivo* tissues (fat, glandular, malign tumor, vascular tissue etc.) is higher for microwaves. It has been reported high contrast of dielectric properties between fibro glandular tissues and tumor tissues in breasts and that it is a non-ionizing method which probably will be rather inexpensive [4].

For this reason, microwave imaging has been developed and has the potential to be a complementary modality to standard mammography. However, it remains a field with many uncharted domains, and microwave imaging techniques need to overcome many challenges and be improved. This includes the enhancement of both more sophisticated hardware (antenna, electromechanical parts, and RF-design) as well as in the software (imaging algorithms) to be considered as a reliable modality for biomedical application.

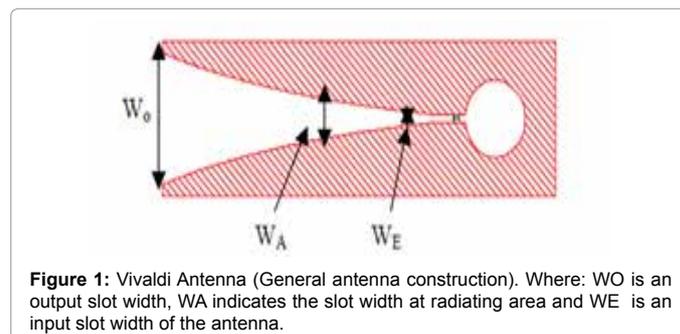
## Design, Materials and Methods

Vivaldi type is one type of a traveling-wave antenna of the "surface-type". Besides being efficient and lightweight, Vivaldi antennas have more attractive features, that they can work over a large frequency bandwidth and produce a symmetrical end-fire beam with appreciable gain and low side lobes [5]. Figure 1 depicts the construction of a Vivaldi antenna.

## Antenna design

The immobilized Microstrip-fed Vivaldi antenna design is based on the parameter study so that the wideband performance could be improved in a systematic procedure. The parametric study and design of a microstrip-fed vivaldi antenna is calculated following selection of the substrate material, substrate thickness, antenna length, antenna width and the slotline width. As the electrical length of the antenna increases with frequency the gain increases.

Antenna performance (S11 and pattern) was discussed basing on the effect of varying these parameter values. Particularly, it was found out that through proper change in the



**Figure 1:** Vivaldi Antenna (General antenna construction). Where: W<sub>0</sub> is an output slot width, W<sub>A</sub> indicates the slot width at radiating area and W<sub>E</sub> is an input slot width of the antenna.

**\*Corresponding author:** Samira Al'Habsi, Department of Electronics and Communication, Middle East College, Al'Rusayl-Muscat, Sultanate of Oman, Tel: +968 96358867; E-mail: [samira.alhabsi.1991@ieee.org](mailto:samira.alhabsi.1991@ieee.org)

**Received** December 21, 2016; **Accepted** December 23, 2016; **Published** December 28, 2016

**Citation:** Al'Habsi S, Al'Ruzaiqi T, Al'Hadharami K, Gopinathan ST (2016) Development of Antenna for Microwave Imaging Systems for Breast Cancer Detection. J Mol Imag Dynamic 6: 128. doi:10.4172/2155-9937.1000128

**Copyright:** © 2016 Al'Habsi S, et al. This is an open-access article distributed under the terms of the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original author and source are credited.

design parameters, the antenna resistance could be increased. For the design of the antenna, TLC-32 substrate with a dielectric constant of 3.2 is selected. Effective thickness of the dielectric substrate ( $t_{eff}$ ) is defined as follows:

$$\frac{t_{eff}}{\lambda_o} = (\sqrt{\epsilon_r - 1}) \frac{t}{\lambda_o} \quad (1)$$

Where,  $\lambda_o$  is the free space wavelength at the center frequency,  $t$  is the thickness and  $\epsilon_r$  is the dielectric constant of the substrate. The essential criteria for any TSA to possess travelling wave antenna characteristics is defined as:

$$0.005 \leq \frac{t_{eff}}{\lambda_o} \leq 0.003 \quad (2)$$

In order to achieve a transition that has low return loss over a wide frequency band, the impedances of the micro strip line and the slot line must be matched to each other to reduce the reflections. The characteristic impedance of a slot line increases with increasing slot width, so the width of slot line must be selected to be as small as possible to achieve a small impedance value. The width, characteristic impedance, and guided wavelength of slot line are calculated with procedures suggested in [6-8]. Hence the antenna parameters calculated are as given in Table 1.

### Micro-strip-fed Vivaldi antenna layout

**Method:** All Tapered-slot antennas are frequently etched with other components onto the same dielectric substrate. The Microstrip-fed Vivaldi has the advantage over other TSA that it can easily be integrated in the circuit. The microstrip to slotline transition is realized by etching the slotline on one side of a substrate. On the opposite side of the substrate, a microstrip line crosses below and perpendicular to the slotline. After crossing below the slotline, the microstrip line is flared to form a radial stub which acts as a wideband, virtual short circuit. Antenna Magus has taken care of this non-trivial design process and includes the designed feed section detail in the antenna model.

The main field of the project is a research approach to select the most optimum antenna that meets requirements of microwave imaging. Antenna Magus and CST Microwave Studio Simulator are proposed for simulation purpose. This software is given great flexibility in tackling a wide application range multi-frequency antennas, it offers both low frequency operation as well as a high frequency bandwidth and operating bandwidth. Imaging systems need to work on different operating frequency and pattern. There are many methods of designing multi-frequency antenna.

The proposed model is designed using the guided wave traveling in the slot transmission line (slotline) and the plane wave, which is radiated. This transition is achieved by a gradual tapering of the slotline. In Vivaldi with a microstrip feed, the microstrip line is printed on a substrate and the tapered slotline is etched on the ground plane below the microstrip. A few parameters are of great importance for satisfactory wideband performance: The length and the width of the tapered slot line: to achieve the traveling wave mode of radiation, the slot length and width generally needs to be greater than and, respectively (Figures 2-4) [9].

### Simulation results

The nanoscope Simulations were done through Antenna Magus Software with Vivaldi design dimensions as described. Various simulations were done to better tune the operating frequency required for microwave imaging that it should be an Ultra-Wide-Band. The results represent final simulations (Table 2).

| Name         | Description  | Value         |
|--------------|--|---------------|
| Hf           | Flare height   | 19.87 mm      |
| Lf           | Flare length   | 37.93 mm      |
| Hc           | Height of the conductor                                      | 25.28 mm      |
| Dc           | Cavity diameter  | 2.598 mm      |
| Smc          | Distance form cavity to the centre of the microstrip coupler | 223.9 $\mu$ m |
| Lmc          | Length of microstrip coupler                                 | 2.598 mm      |
| Wmc          | Width of microstrip coupler                                  | 447.8 $\mu$ m |
| Lmt          | Length of tapered microstrip line                            | 6.700 mm      |
| Wmt          | Width of the tapered microstrip line at the port             | 1.900 mm      |
| Ls           | Length of slotline   | 447.8 $\mu$ m |
| Ws           | Width of the slotline  | 464.8 $\mu$ m |
| Rs           | Radius of the microstrip stub                                | 2.074 mm      |
| $\Theta_s$   | Starting angle of the microstrip stub                        | 90°           |
| $\Theta$     | Angle of the microstrip stub                                 | 80°           |
| Hs           | Substrate height   | 790 $\mu$ m   |
| $\epsilon_r$ | Dielectric constant of the substrate                         | 3.2           |
| Tan $\delta$ | Loss tangent of the substrate                                | 0             |
| Ft           | Factor determining the opening rate of the flare             | 83            |

Table 1: Designed parameters of the antenna.

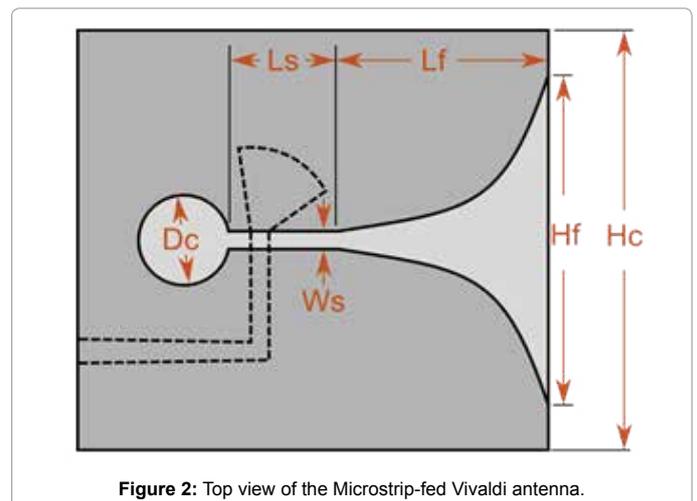


Figure 2: Top view of the Microstrip-fed Vivaldi antenna.

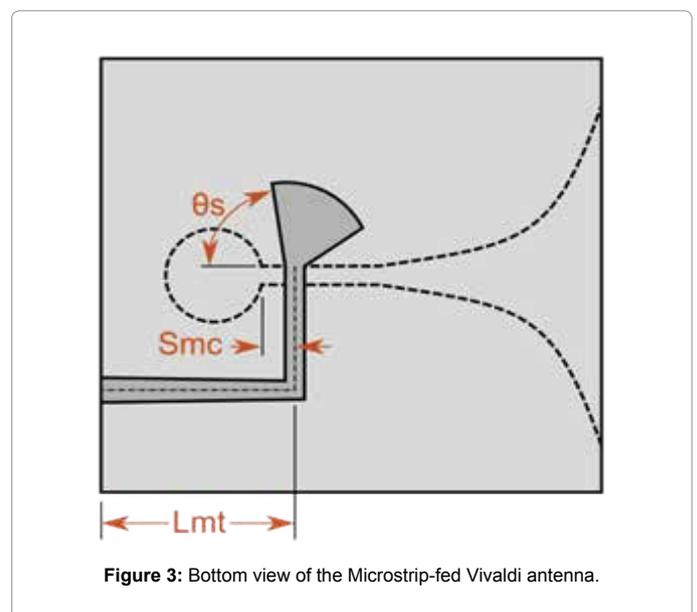


Figure 3: Bottom view of the Microstrip-fed Vivaldi antenna.

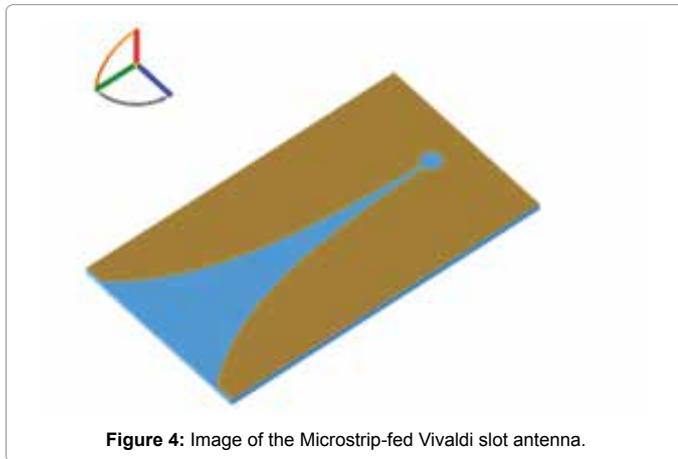


Figure 4: Image of the Microstrip-fed Vivaldi slot antenna.

| Name                  | Description  | Value   |
|-----------------------|--|---------|
| Fmin                  | Minimum frequency                                      | 8.3 GHz |
| Name                  | Substrate: The substrate name.                         | TLC-32  |
| Manufacturer          | Substrate: The substrate manufacturer.                 | Taconic |
| Substrate Thickness   | Substrate: The thickness of the substrate.             | 790 μm  |
| Relative Permittivity | Substrate: The relative permittivity of the substrate. | 3.2     |

Table 2: Summary of the substrate chosen to fit into microwave imaging systems.

### Estimated performance charts

Human In (Figure 5), the simulated variation of the antenna input impedance versus frequency of the proposed Microstrip-Fed Vivaldi antenna can be seen. At the operating frequency of approximately 8.3 GHz, the average value of the resistance (real part) is about 140 Ohms and the average value of the reactance (imaginary part) is approximately 40-Ohms which gives the adequate input impedance matching at the desired resonant frequency.

The input impedance is as summarized in the following (Table 3):

The reflection coefficient ( $|S_{11}|$ ) (dB) of the proposed antenna provides a good matching input impedance with a good return loss of less than -10 dB at operating bandwidth of (7.143-24.60) GHz, and having the reflection coefficient of -37.56 dB at 18.39 GHz as depicted in Figure 6.

The minimum voltage standing wave ratio, VSWR of 1.02 is observed at frequency of 18.39 GHz, and having a VSWR of 2 at a bandwidth of approximately 7-24 GHz indicating low power return at the frequency of operation.

Table 4 is a summary of Smith Chart simulated results of Microstrip-Fed Vivaldi Antenna.

### Antenna testing and evaluation

The designed antenna is fabricated and tested. It is important to note the difficulty involved during antenna fabrication and when taking its measurements. Since several expensive test components are needed, along with a suitable test component to test the antenna at higher frequency bandwidth, thus the frequency of operation designed and simulated is lowered for ease of fabrication. In this case, a lower frequency range of 2.4 GHz is included. The test component used for antenna testing is (the HP 8753D Network Analyzer). Because of this, simulation results were used to compare actual test results for accuracy at higher frequencies and results after fabrication indicates better results

at lower frequencies. The following test results shows data involved a 2.4 GHz Microstrip-Fed Vivaldi Antenna using FR-4 substrate with 4.4 dielectric constant. The plot of Figures 7a and 7b, shows the top and bottom geometry of the antenna along with its dimensions.

### Antenna specifications

Frequency of operation = 2.4GHz

FR4 Material dielectric constant = 4.4

Thickness=1.6 mm

Total dimension=85.8 mm ×130 mm

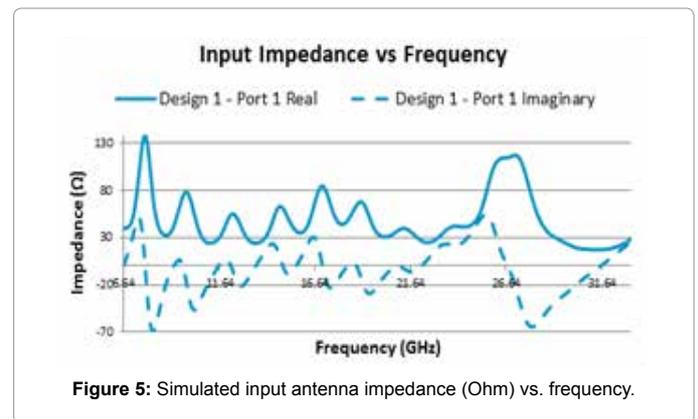


Figure 5: Simulated input antenna impedance (Ohm) vs. frequency.

|  |                     |
|--|---------------------|
| Peak real impedance @ frequency          | 138.1 Ω @ 7.730 GHz |
|  | 138.1 Ω @ 7.752 GHz |
|  | 42.84 Ω @ 9.259 GHz |
|  | 74.41 Ω @ 9.729 GHz |
|  | 28.79 Ω @ 11.59 GHz |
|  | 53.98 Ω @ 12.24 GHz |
|  | 24.12 Ω @ 13.54 GHz |
| Real impedance @ zero-crossing frequency | 61.84 Ω @ 14.96 GHz |
|  | 37.31 Ω @ 15.64 GHz |
|  | 84.80 Ω @ 17.03 GHz |
|  | 47.87 Ω @ 18.33 GHz |
|  | 63.59 Ω @ 18.81 GHz |
|  | 26.74 Ω @ 22.22 GHz |
|  | 114.9 Ω @ 26.72 GHz |
|  | 17.30 Ω @ 31.59 GHz |
| Mean real impedance                      | 48.66 Ω             |
| Mean imaginary impedance                 | -3.925 Ω            |

Table 3: Input impedance versus frequency.

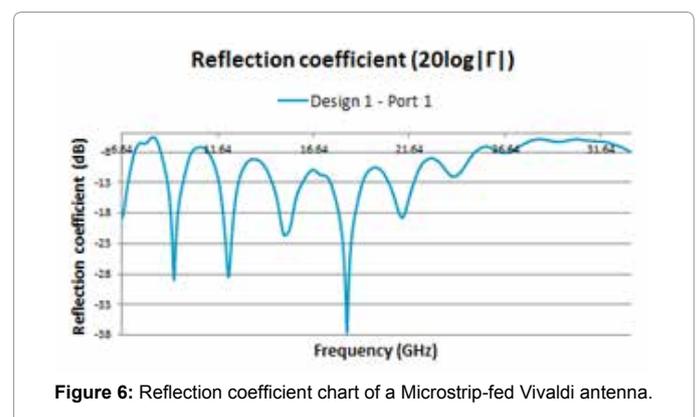


Figure 6: Reflection coefficient chart of a Microstrip-fed Vivaldi antenna.

The design of proposed antenna design is as shown below (Figures 7a and 7b).

**CAD views:** Coaxial feed (shown by green line) is chosen as per 50-Ohm line. The coaxial feed is given 62 mm on x- axis which gives good impedance matching.

### Results

The gain of the antenna under test is measured in the bore sight direction. The experimental setup to determine antenna gain is similar to the radiation pattern measurement setup. After fabrication, the antenna is found to have a gain of 2.5 dB at the frequency of operation 2.4 GHz as depicted in Figure 8.

Scatter parameter S11 (The return loss) for the antenna is as depicted by Figure 9. Ideally, the amount of reflection should be at a minimum for the antenna design frequency (2.4 GHz). Taking a look at the illustration, the least amount of reflection occurs at exactly 2.4 GHz, in which the return loss at minimum of -26.34 dB.

From the graph of Figure 10, the minimum voltage standing wave ratio, VSWR of approximately 1.1 is observed at frequency of 2.4 GHz, and having a VSWR of below 2.4 at a bandwidth of approximately 2.2-2.8 GHz indicating low power return at the frequency of operation.

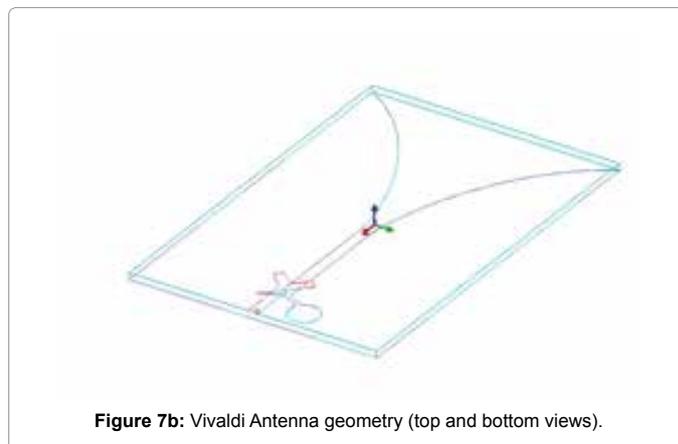


Figure 7b: Vivaldi Antenna geometry (top and bottom views).

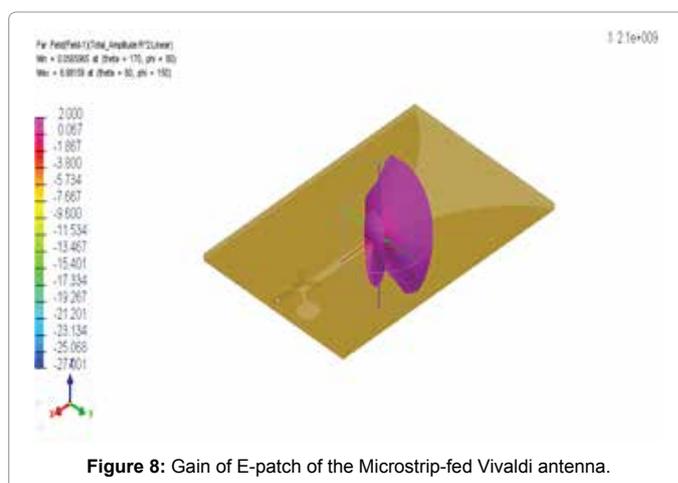


Figure 8: Gain of E-patch of the Microstrip-fed Vivaldi antenna.

|                              |           |
|------------------------------|-----------|
| Frequency at which VSWR = 2  | 7.175 GHz |
|                              | 8.786 GHz |
|                              | 10.09 GHz |
|                              | 11.39 GHz |
|                              | 13.21 GHz |
|                              | 13.86 GHz |
|                              | 22.43 GHz |
|                              | 23.15 GHz |
| 24.69 GHz                    |           |
| Minimum VSWR value           | 1.027     |
| Reference impedance @ port 1 | 50 Ω      |

Table 4: Summary of Smith chart simulated results of Microstrip-Fed Vivaldi Antenna.

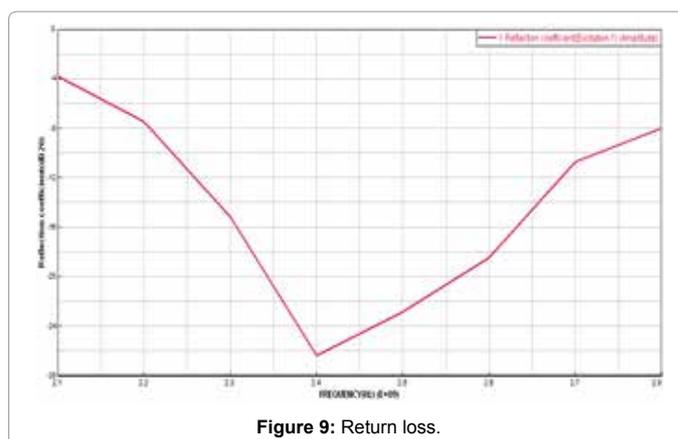


Figure 9: Return loss.

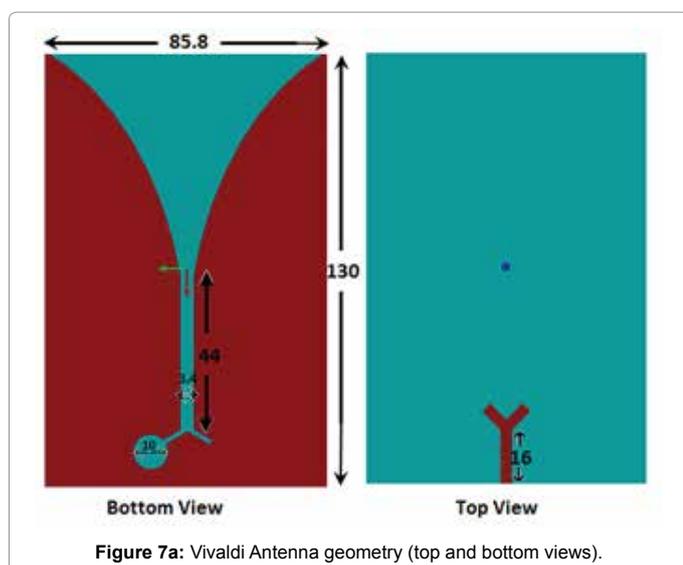


Figure 7a: Vivaldi Antenna geometry (top and bottom views).

Figure 11 is plot representing how 2D radiation pattern would appear. Test results indicates a unidirectional (directive) radiation pattern as per the requirement of antenna suitable in microwave imaging for breast cancer detection.

### Conclusions and Recommendations

The results of the antenna simulation and test results after fabrication were overall very pleasing. Development of antenna for microwave imaging systems for breast cancer detection project was a research based in which various antennas were designed and

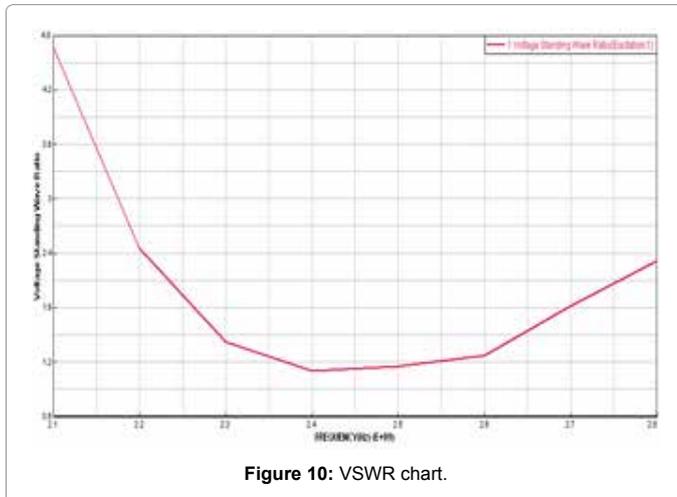


Figure 10: VSWR chart.

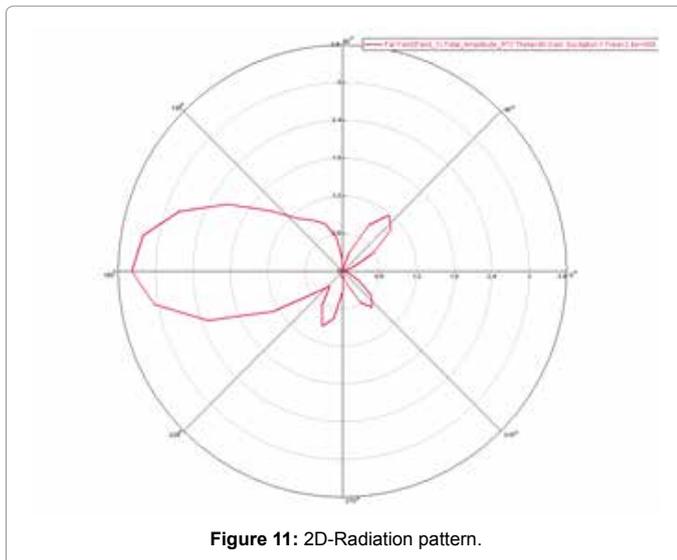


Figure 11: 2D-Radiation pattern.

simulated. Among Microstrip patch antenna and fractal antennas, Microstrip-Fed Vivaldi antenna was found to present the most suitable results for imaging systems. It was quite easy to design, simulate and fabricate. The fabrication and testing phase of the project was the most difficult. The difficulty in taking measurements that was significantly underestimated. The major setback during the entire period of the project was the fact that our labs are not furnished with all the necessary antenna test equipment that we can fabricate the antenna at higher frequency as expected after simulations. It eventually was discovered that some antenna measurements including the frequency of operation could be made with reasonable accuracy with the current test equipment and environment available. Mainly, it was possible to measure the impedance match of a test antenna, along with an abstract plot of the characteristic of the antenna including radiation property, gain, return loss and VSWR. Taking into consideration the amount of time and hard work this project required, the results are extremely pleasing. The department is now in a reasonable position to develop a complete antenna design at higher frequencies when equipment are available in our lab.

Both TLC-32 and FR-4 substrates offers some amount of flexibility making them suitable for breast cancer detection to easily detect breast

tissues. These substrates were chosen based on availability in the market.

It is recommended that for enhancing bandwidth and reducing return loss, antenna can be designed by using different flexible substrates when available. Antenna performance can also be altered by using different feeding techniques.

## Notes

This project research and publication were funded by the Research Council of Oman, TRC as a part of "Faculty Mentored Undergraduate Research Award Program, FURAP". The research work is also supported by Middle East College, Department of Electronics and Communication Engineering, Al'Rusaiyl. Any discussion, results, findings, conclusions or recommendations expressed in this report are those of the authors.

## Acknowledgments

The authors would like to thank the Research Council of Oman, TRC and Middle East College for funding this research work with whom all valuable resources to support this work have been possible.

Specifically, they would like to express gratitude to Ms. Sreelakshmi T. Goopinathan and Dr. Elizabeth Rufus for their exemplary guidance and constant encouragement to research on this area.

## References

1. Bhattacharya DD (2012) Ultra wide band microstrip patch antenna design for wireless application. International Journal of Engineering Research & Technology 1: 1-4.
2. Poplack SP, Tosteson TD, Wendy AW, Pogue BW, Meaney PM, et al. (2007) Electromagnetic Breast Imaging: Results of a pilot study in women with abnormal mammograms. Radiology 243(2): 350-359.
3. Fear EC, Bourqui J, Curtis C, Mew D, Docktor B, et al. (2013) Microwave breast imaging with a monostatic radar-based system: A study of application to patients. Microwave Theory and Techniques 61(5):2119-2128.
4. Grzegorzczuk TM, Meaney PM, Kaufman PA, Di Florio-Alexander RM, Paulsen KD (2012) Fast 3-D tomographic microwave imaging for breast cancer detection. Medical Imaging 31(8): 1584-1592.
5. Gibson PJ (1979) The Vivaldi Aerial. Proceedings of the 9th European Microwave Conference. 103-105.
6. Janaswam R, Schaubert DH (1986) Characteristic impedance of a wide slot line on low permittivity substrates. IEEE Transactions on microwave theory and techniques 34(8): 900-902.
7. Adnan S, Abd-Alhameed RA, Hraga HI, Elfegani ITE, Noras JM, et al. (2011) Microstrip antenna for microwave imaging application. Electromagnetics Research Symposium Proceedings. Marrakesh, Morocco, 20-23.
8. Sivaranjani, Pavani P, Venkatesh S, Nagaraju GS, Nagamadhavi D (2014) Circular micro strip antenna design for ultra-wideband. International Journal of Engineering Science & Advanced Technology 3(3): 176-182.
9. Sharma M, Jindal P, Chahar S (2014) Design of fractal antenna for multiband application. International Journal of Advanced Research in Computer Science and Software Engineering 4(6): 854-858.

Citation: Al'Habsi S, Al'Ruzaiqi T, Al'Hadharami K , Gopinathan ST (2016) Development of Antenna for Microwave Imaging Systems for Breast Cancer Detection. J Mol Imag Dynamic 6: 128. doi:10.4172/2155-9937.1000128