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Silica-Supported Bimetallic Co-Cu Composite - An Efficient Catalyst for Ethanol Based Hydrogen Production by Steam Reforming Technique

Zelalem Tekulu, Yadav OP* and Tesfahun Kebede

Department of Chemistry, Haramaya University, Dire Dawa, Ethiopia

Abstract

During the last few decades, there has been a growing interest in developing alternative energy systems to fossil fuels. Steam reforming of ethanol for producing hydrogen gas is promising since ethanol can readily be obtained through bio-mass fermentation. In the present work, catalytic activity of silica-supported bimetallic Co-Cu composites, for hydrogen production by steam reforming of ethanol, has been studied. A fixed-bed reactor was used to assess the performance of composite catalysts over the temperature range: 300-600°C. Catalyst activity, using varying water:ethanol molar ratio, was evaluated in terms of hydrogen yield and product selectivity. Ethanol conversion, hydrogen yield and selectivity were found to increase on raising water: ethanol molar ratio, catalyst load and the Co:Cu ratio. The catalyst with composition 8% Co/4% Cu/SiO2 at water:ethanol ratio 9:1 and temperature 500°C, gave ethanol conversion as high as 97.2%.

Keywords: Bimetallic; Composites; Catalysts; Conversion; Steam

Introduction

In the recent years, there has been a growing interest in developing alternative energy systems to fossil fuels. Hydrogen gas - a viable energy carrier for the future [1,2], is being used in fuel cells for generating electricity, with high efficiency. Hydrogen represents a promising fuel since it is considered as a clean energy carrier and also because during its combustion only water is emitted. As hydrogen can be produced from different kinds of renewable feedstocks, such as ethanol, therefore, hydrogen could be treated as biofuel. Chemical reactions involved in the production of hydrogen from ethanol are: steam reforming (SR), partial oxidation (POX), and autothermal reforming (ATR) [3]. Among a range of possible sources to generate hydrogen gas, the steam reforming of methane, covers about 50% of the world's feedstock for hydrogen production [4]. Steam reforming of ethanol for producing hydrogen gas is a promising means since ethanol can readily be obtained through bio-mass fermentation. Further, besides being more safe and easier to handle, steam reforming of ethanol occurs at comparatively lower temperature compared to other fuels [5,6].

During reforming process of ethanol, besides, the main products: H₂ and CO₂, biproducts such as CO and CH₄ are also formed [7-9]. The reaction pathway of ethanol steam reforming depends on the reaction conditions such as nature of catalyst and temperature which significantly affect the H₂ production. The selection of a suitable catalyst plays a vital role in ethanol steam reforming reaction leading to H₂ production [9]. Earlier, Batista et al. [10] studied steam reforming of ethanol using Co/ Al₂O₂ and Co/SiO₂ catalysts with a cobalt content of 8 and 18% (w/w), respectively. The catalysts showed average conversion higher than 70% for the steam reforming of ethanol at 400°C. Cussins et al. [11] have reported that copper/nickel/Alumina composite catalyst can yield 1.3 moles hydrogen per mole ethanol reacted at 300°C and atmospheric pressure with excess water in the feed solution. Ciambelli et al. [12] investigated Catalytic activity, selectivity and stability of a Pt/CeO, (5 wt% Pt) catalyst in the low temperature ethanol steam reforming reaction for hydrogen production and could achieve complete ethanol conversion at 300°C with negligible CO, Dan et al. [13] investigated effect of support modification on hydrogen production by ethanol steam reforming on nickel catalysts. They observed that the promotion of both alumina and zirconia with CeO₂ and La₂O₃ lead to changes in the Ni - support interaction resulting in much better dispersion and stabilization of the Ni nanoparticles on the catalyst surface. For La_2O_3 promoted catalysts 100% ethanol conversion was obtained at temperatures as low as 300°C.

Veiga et al. [14] investigated production of H_2 -rich gaseous mixtures from steam reforming of crude glycerol on ternary Ni–La– Ti catalysts. Standard catalytic tests for the steam reforming of glycerol were performed at 500°C or 650°C by feeding the fixed-bed tubular reactor with a crude glycerol:water solution containing 30 wt% glycerol. Recently, Hakkel et al. [15] has presented a model system consisting of Ni particles grown onto epitaxial CeO₂ films, deposited on CaF₂-buffered Si(111), for molecular level study of the transformations of ethanol under steam reforming conditions. They have explored adsorption behaviour of ethanol and other stable compounds, important in ethanol reforming, by means of photoelectron spectroscopy.

It is believed that the use of composite transition metals catalysts, supported on a suitable metal oxide, can significantly inhibit undesirable ethanol dehydration and thus can enhance steam reforming of ethanol [7]. In the present study, we have used bimetallic Co-Cu/SiO₂ composite catalysts of varying composition, for the steam reforming of ethanol. Effects of operational parameters such as: catalyst load, temperature, composition of active phase and water to ethanol molar ratio, have been investigated.

Materials and Methods

Chemicals

Cobalt nitrate hexahydrate [Co(NO₃)₂.6H₂O, Blulux], copper

*Corresponding author: Yadav OP, Department of Chemistry, Haramaya University, Post Box 138, Dire Dawa, Ethiopia, Tel: +918059602660; E-mail: yadavop02@yahoo.com

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nitrate trihydrate $[Cu(NO_3)_2.3H_2O, Merck]$, Argon (Afro German Chemicals) and silica (Fisher) and ethanol (C_2H_5OH , Park) were of analytical grade.

Catalytic reactor

Schematic design of steam reforming reactor system in Figure 1. The reactor tube is made of steel (length: 25 cm and internal diameter 1.27 cm). Catalyst was loaded over a quartz wool kept over metal grating at the centre of the reactor tube. A tubular furnace made of clay (embedded with glass-wool) surrounding the reactor tube was designed to achieve temperature upto 600°C.

Methods

Preparation of catalysts: Silica (SiO_2) based bimetallic Co-Cu composite catalysts were prepared by mixing the former with $Co(NO_3)_2.6H_2O$ and Cu $(NO_3)_2.3H_2O$ salts in desired proportions by impregnation method. Stoichiometric amounts of cobalt and copper salts were, separately, dissolved in de-ionized water. The two solutions of the precursor salts were thoroughly mixed and then appropriate amount of silica powder was added to it. The slurry was heated in an evaporating dish at 140°C for 12 hours. The dried composite catalyst was calcined at 550°C for 5 hours and the product was stored at room temperature in moisture-free atmosphere.

Evaluation of the catalytic performance: Composite catalyst (1.4 g) was loaded over a thin layer of quartz wool in the reactor tube (Figure 1). After the desired operational temperature was reached, argon gas was allowed to flush through the reactor tube for 5 minutes. Water+ethanol solution of desired molar ratio (3:1, 6:1 or 9:1) was allowed to enter at one ml/min into the evaporator tube kept at 200°C. Ethanol and water vapors, mixed with the argon gas at flow rate: 20 ml/min, were fed into the reactor tube at atmospheric pressure. The reaction was carried out over the temperature range: 300 to 600°C. The gaseous products were cooled down to room temperature and collected in gas sample bags. The gaseous samples were analyzed using Permselective Gas Sensor equipped with non-dispersive I.R. detector.



Physical state: As-synthesized composite catalysts were powders of different colors due to difference in moler ratio of their active

of different colors due to difference in molar ratio of their active phases. Whereas, pre-calcined SiO_2 -based Co-Cu composite catalysts, containing higher load of cobalt, had reddish color, the catalysts containing higher load of copper were bluish in color. Upon calcinations at 550°C, the catalysts turned grey in color. The grey color of catalyst further intensified and turned black upon increasing the cobalt load.

Evaluation of catalytic performance

Results and Discussion

Characterization of catalyst

Performance and activity of a catalyst can be evaluated in terms of parameters such as: percent conversion of ethanol, $X_{EtOH}(\%)$, percent H_2 yield, $Y_{H2}(\%)$, percent H_2 selectivity, $S_{H2}(\%)$, percent CO_2 selectivity, $S_{CO2}(\%)$, and percent other products selectivity, $S_{others}(\%)$, calculated using the following expressions [8,16].

$$X_{EIOH}(\%) = \left(\frac{\text{Ethanol in - Ethanol out}}{\text{Ethanol in}}\right) \times 100$$
(1)

$$Y_{H_2} (\%) = \frac{\text{moles } H_2 \text{ produced}}{\text{moles EtOH reached}} \times \frac{1 \text{ mole EtOH}}{6 \text{ moles } H_2} \times 100$$
(2)

$$S_{CO_2}(\%) = \frac{CO_2 \text{ out}}{H_2 \text{ out} + CO_2 \text{ out} + \text{Others out}} \times 100$$
(3)

$$S_{CO_2}(\%) = \frac{CO_2 \text{ out}}{H_2 \text{ out} + CO_2 \text{ out} + \text{Others out}} \times 100$$
(4)

$$S_{others}(\%) = \frac{Others out}{H_2 out + CO_2 out + Others out} \times 100$$
(5)

Effect of total catalyst load and Co:Cu ratio on catalytic performance: Percent ethanol conversion, X_{EtOH} (%) and percent hydrogen yield, Y_{H2} (%) as a function of total load of Co+Cu at one atmospheric pressure, temperature 500°C and H_2O/C_2H_5OH molar ratio 3:1 is shown in Figure 2. Whereas, percent H_2 yield increases with the increase of total load of the catalyst, over the entire studied catalyst load, percent ethanol conversion attains a limiting value at total catalyst load 8 g. Further, composite catalysts having the same total load of active phases but with higher Co:Cu ratio led to higher percent ethanol conversion as well as hydrogen yield (Figure 3).

Percent selectivity of hydrogen, carbon dioxide and other products: Percent H₂ selectivity, $S_{H2}(\%)$, percent CO₂ selectivity, $S_{CO2}(\%)$, and percent other products selectivity, $S_{others}(\%)$, as a function of total load of Co-Cu and Co:Cu ratio are presented in Figures 4 and 5 respectively. At the given temperature (500°C) and H₂O:C₂H₃OH ratio (3:1), whereas, with the increasing Co-Cu load as well as Co:Cu : ratio, % selectivity of both H₂ and CO₂ increases, the reverse is true for the % selectivity of other products of the reaction.

Effect of temperature on catalytic activity: Plots of percent ethanol conversion as a function of temperature at varying composition of catalyst are presented in Figure 6. Ethanol conversion increases with increase of temperature as well as the active catalyst concentration. It is obvious since the overall reaction involved in the ethanol reforming process is of endothermic in nature. The optimum temperature for ethanol conversion 500°C. At still higher temperature, 600°C, there was no further gain in percent ethanol conversion. Below 500°C, owing to the dehydrating nature of the support (Silica), ethanol preferably converts to ethane and water, resulting in the decrease of hydrogen production. Also, at low temperatures enough energy is not

bag.

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Figure 2: Percent ethanol conversion, X_{EtOH} (%) and percent hydrogen yield, Y_{H2} (%) at 500°C as a function of total load of Co+Cu (P=1 atm; H₂O/C₂H₅OH molar ratio:3:1).



Figure 3: Percent ethanol conversion (X_{EIOH} %) and Percent hydrogen yield (Y_{μ_2} %) *versus* Co:Cu ratio; at 500°C, (P=1 atm., H₂O/C₂H₅OH molar ratio 3:1).



Figure 4: Percent H₂ selectivity, S_{H2}(%), percent CO₂ selectivity, S_{CO2}(%), and percent other products selectivity, S_{others} (%), at 500°C as a function of total load of Co+Cu. (P=1 atm; H₂O/C₂H₅OH molar ratio:3:1).



Figure 5: Percent H₂ selectivity, S_{H2}(%), percent CO₂ selectivity, S_{CO2}(%), and percent other products selectivity, S_{others} (%), at 500°C as a function of Co:Cu ratio; (P=1 atm; H₂O/C₂H₄OH molar ratio:3:1).





available for the decomposition of ethanol- a prerequisite for hydrogen production. The sequence of chemical reactions involved in steam reforming process [16] is given below:

C ₂ H ₅ OH+H ₂ O	$\rightarrow CH_4 + CO_2 + 2H_2; \Delta H^{\circ}_{298K}$	=-8.0 KJmol ⁻¹
$CH_4 + H_2O$	\rightarrow CO+3H ₂ ; Δ H° _{298K}	=+206.1 KJmol ⁻¹
CO+H ₂ O	\rightarrow CO ₂ +H ₂ ; Δ H° _{298K}	=-41.2 KJmol ⁻¹
$C_2H_5OH+3H_2O \rightarrow 2CO_2+6H_2; \Delta H^0_{_{298K}}$		=+156.9 KJmol ⁻¹

Effect of water:ethanol ratio: Percent hydrogen yield and % selectivity of hydrogen, carbon dioxide and other products over 8% Co/4% Cu/SiO₂ composite catalyst at varying water:ethanol molar ratio, are exhibited in Figure 7. Percent yield as well as selectivity of H₂ increases with the increase in water:ethanol ration. Whereas, percent selectivity of other products decreases the selectivity of CO₂ is unaltered with the increase in H₂O:C₂H₅OH ratio. These results conform with the

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Figure 7: Percent hydrogen yield (Y_{H2}) . Hydrogen selectivity (S_{H2}) , carbon dioxide selectivity (S_{co2}) and other products selectivity (S_{others}) over 8%Co/4%Cu/SiO₂ composite catalyst and at varying water:ethanol molar ratio (temperature: 500°C and P:1 atm).

works reported by Umegaki et al. [9] and Bergamaschi and Carvalho [17] who had used 20% Ni/SiO₂, 5% Pd/In₂O₃ and 2% Cu/5% Ni/ ZrO_2 catalysts, respectively, while studying ethanol steam-reforming process. Though a wide variety of base metals such as Ni, Cu, Co or noble metals like Rh, Pt and Ru, deposited on suitable support material, have been used by other workers as reviewed by Bineli et al. [3], yet no comparison could be made with them as the catalysts used in our work are different.

Conclusion

Activities of silica (SiO_2) -supported Co-Cu composite catalysts, with varying composition, for the production of H₂ gas, in the ethanol steam reforming process, have been studied. Effects of water:ethanol ratio, catalytic load, Co:Cu load ratio and temperature on ethanol conversion, hydrogen yield and reaction products selectivity have been investigated. Higher water:ethanol ratio, higher Co:Cu load ratio and higher temperature lead to enhanced ethanol conversion, more yield as well as selectivity of hydrogen gas. The catalyst having composition: 8% Co/4% Cu/SiO₂ performed best with 97.15% ethanol conversion at optimum temperature 500°C and water ethanol ratio 9:1. No comparison could be made with the previously reported works as the catalysts used in our work were different from those reported by other workers.

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